Design of ring VCO based PLL using 0.25 µm CMOS technology

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Abstract— A low power ring VCO based PLL using injection locking is realized by adopting 0.25µm CMOS technology at 2.5V. We have achieved a shift in the bias level by using pMOS active resistive load. The PLL output frequency is 104.4 MHz, at 5 MHz reference frequency by using injection locking based VCO and active resistive load managed to achieve low power dissipation of 4.98mW at 2.5 V.

Index Terms- Phase Locked Loop, Injection Locking, Ring VCO, Shift Bias Level.

I. INTRODUCTION

PLL is very important building block used in communication, computers and other digital systems. Many digital devices such as Mobile phone, Notebooks operates at very high frequencies for which PLL are used for frequency synthesis, all these devices works on batteries so it becomes very important to design systems which consumes less power. The objective of this dissertation is to design a low power CMOS PLL at 2.5 V using 0.25 μm . In this paper we are designing a VCO using the MOS capacitance and active load resistance which are scalable, consumes less power and occupies less area. Also we are using Injection locking VCO to reduce the phase noise. This paper is organized as follows. Section 2 describes the design of differential injection locked ring VCO and all the necessary building blocks. Section 3 contains the comparison of the work done in this paper. The results are discussed in Section 4 along with the conclusion.

We have used injection locking as there are no stability issues and it also increases the loop bandwidth. The output phase noise tracks injection signal phase noise over wide bandwidth and it is very easy to implement. Injection locking can be used at very high frequencies.

II. DESIGN OF THE DIFFERENTIAL INJECTION-LOCKED RING-VCO

Usually tuning exhibits nonlinearity i.e. K_{VCO} is not constant. Such nonlinearity degrades the settling behavior of PLLs and leads to high sensitivity for some frequency region. To avoid this we need to minimize the variation of K_{VCO} across the whole tuning range. The linearity of the frequency tuning of a VCO is easily seen from its functional dependence of K_{VCO} on the control voltage. The closed loop transfer function of a PLL, H(s) is proportional to K_{VCO} . The loop bandwidth is given as:



where Ip is the charge pump current, N is the division ratio of the feedback loop, and C_f is the filter capacitance. So we can see that the loop bandwidth can be changed by varying the K_{VCO} [11]



Fig. 1. Proposed differential delay cell[1]



Fig. 2. Schematic and transfer characteristics of bias level shifter [1]





Control voltage for VCO is generated by charge pump which passes through the RC filter the transient response of control voltage to VCO is shown above. This response shows that VCO control voltage varies linearly with time.



Fig. 4.Transient response of voltage control voltage for VCO



Fig.5.Transient response of VCO with T = 9.63 ns and f=104.4 MHz



Fig. 6.Schematic of PFD

PFD compares the phase of two input signals one is the clock frequency or reference signal and other is the feedback signal from VCO to frequency divider and to PFD. PFD output is fed to the charge pump circuit. It has two inputs A and B which is applied to the clock terminal of the D flip flop.



Fig. 7.Transient response of PFD Charge pump circuits are capable of high efficiencies, (90–95%) while being electrically simple circuits.



Fig. 8.Schematic of CMOS charge pump based on the current mirror technique

A divide by two circuit commonly called DTC is widely used to produce quadrature outputs.



Fig. 9.Schematic of frequency divider



Fig. 10. Transient response of frequency divider



Fig. 11.Simulation setup of PLL with reference frequency of 5 MHz [1]



Fig.12. (a) Output response of PLL 104.4 MHz (b) Control voltage for VCO (c) Output response of

frequency divider (d) Reference input signal of 5 MHz

The transient response of the PLL is shown in the figure 6.4 which involves reference signal, VCO output frequency, VCO control voltage, and f/2 output signal which is fed to the PFD.

Fig. 13.Magnified transient response of PLL tested at 4 MHz input reference frequency

In this test setup PLL consumes 4.98 mW at 2.5 V power supply. Its transient power consumption curve is shown below

Fig. 13.Transient power consumption cure of PLL (4.98 mW) at 2.5 V power supply

III. PERFORMANCE SUMMARY OF PLL

TABLE 1

I enformance summary of I LL				
0.25 µm CMOS				
process				
2.5 V				
104.4 MHz at 5 MHz				
reference input				
frequency				
4.98 mW				

Performance summary of PLI

IV. CONCLUSION

The design proposed in this dissertation is tested at 5 MHz reference signal but this design can support wide range of reference signal. The purpose of this dissertation is to demonstrate the design at 2.5 V at 0.25 μ m CMOS technology. There are various electronic communication systems which operate at such voltage level. This PLL can be used at the radio receiver and super heterodyne demodulators. Design consumes 4.98 mW at 2.5 V power supply which makes it suitable to use it in battery operated systems. This design can be implemented at different CMOS technology such as 0.18 μ m CMOS technology. Since this design is fully differential, which makes it noise immune.

TABLE 2 PERFORMANCE SUMMARY AND COMPARISON OF PLLs

	Tuning	Phase	Power	CMOS
	range	noise	(mW)	(in nm)
This work	5 MHz		4.98	250

[1]	1.44 GHz	-108	39	180
		dBc/Hz		
[2]	23.8-30.2	-110	31	32
	GHz	dBc/Hz		
[3]	30%	-124.2 at	27.2	32
		23.1 GHz		
[4]	3.5 GHz-	-105		90
	7.1 GHz	dBc/Hz		
[5]			4.3 at	65
			855	
			MHz	
[6]	22.9 %	-127.3at	64	32
		10 MHz		
		from 24.7		
		GHz		
[7]		-60.5 at	1.5	90
		100 KHz		
[8]	2.17-2.48	-112.77 at	14.4	180
	GHz	1 MHz		
		offset		
[9]	22.9 %	-97.5@	16	65
		1MHz		
[10]	6.35 %	-91.46	7.5	180
		@1MHz		
		offset		

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