

AN ANTI-ISLANDING TECHNIQUE FOR DISTRIBUTION SYSTEMS

R. Vinay Kumar¹, D. Masthan²

¹M.Tech student, EEE,

²Associate professor, EEE,

Dr.K.V.Subbareddy college of Institute & Technology, Kurnool, Andhra Pradesh, India

Abstract- Due to the variety of distribution generation (DG) sizes and technologies connecting to distribution networks, and the concerns associated with out-of phase reclosing, anti-islanding continues to be an issue where no clear solution exists. An exemplification system is constructed by using the standard distribution apparatus and arecluse controller and the distributed generators were tripped through the high-speed communications circuit and were blocked from closing back it is tested on the utility's distribution test line model to a protection. The operation shows anti-islanding detection time is approximately a cycle longer than the delay associated with the application of the auto ground. Once the auto ground is applied, the DG is disconnected within 4 cycles on overcurrent protection and applies to all DG types, the concept is inherently scalable, is confiscable to various reclosing operations and does not require additional equipment or setting changes at the producer's site, and reduces the cost of equipment.

Index Terms- Distributed generation, distribution relaying, renewable energy.

I. INTRODUCTION

Electric power distribution systems have traditionally been designed assuming that the primary substation is the sole source of power and short-circuit capacity. Distributed resources invalidate this assumption by placing power sources onto the distribution system. As a result, DR interconnection results in operating situations that do not occur in a conventional system without generation directly connected at the distribution level. Careful engineering can effectively eliminate the potentially adverse impacts that DR penetration could impress on the electric delivery system, such as exposing system and customer equipment to potential damage, decrease in power quality, decrease in reliability, extended time to

restoration after outage, and potential risks to public and worker safety. There are different system issues which may be encountered as DR penetrates into a distribution system. Load currents through the power and distribution transformer and line impedances cause voltage drops, which reduce voltage magnitude at the loads. Voltage magnitudes at service locations must be maintained within specified ranges. This is accomplished in both fixed designs of the system (e.g., conductor selection, substation and distribution transformer tap settings and fixed capacitor banks) and by voltage control equipments such as automatic load tap changers, step-type voltage regulators (SVR), and switched capacitors.

The fixed design of the feeder is based on the assumption that loading profiles generally follow a predictable pattern, with real power loading on the feeder causing voltage to decrease monotonically from the substation. SVR controls continuously monitor voltages and load currents to adjust tap positions accordingly. Capacitors (switched and fixed) compensate reactive current, reducing the current from the source to the capacitor location, resulting in reduced line voltage drop.

However, capacitors will cause a current increase in feeders if the capacitor size is greater than the load reactive demand due to overcompensation. This will also happen if the capacitor size meets the reactive demand of the total distributed load connected to a feeder, but is installed at a location where it compensates more than the downstream reactive power demand, resulting in voltage increase. When a distributed generation (DG) is interconnected to the distribution system, it can significantly change the system voltage profile and interact with SVR and/or

capacitor control operations. Anti-islanding has been the subject of a number of studies these approaches can be typically divided into the following two classifications: passive approaches using the local measurements of voltage and current, and variables derived from using these quantities, to delineate between islanding and grid connected operation and active approaches where by the DG perturbs the grid voltage or frequency, an approach intended to be benign while the grid is present, and to destabilize the system when the substation is open. A third approach is in fact a variant on communication based approaches, whereby using thyristor valves connected to ground, a disturbance is periodically injected at the substation-its presence at the DG's location indicates a normal condition, whereas its absence is indicative of an islanded grid have also suggested these thyristor based devices for fault identification in. Similar to active islanding techniques, this approach could be criticized alone on the impact on power quality. Additionally, in noisy grids or feeders that are particularly long, the issue of nuisance tripping is an issue.

This paper proposes an approach to anti-islanding protection that is based on applying a three-phase short circuit to the islanded distribution system just prior to reclosing or re-energization. Section II provides the theory and methodology for construction of this utility-owned equipment. Section III presents the experimental set-up and results, and we conclude with a summary of various practical considerations.

II. THEORY AND METHODOLOGY

Anti-islanding protection is required of any distributed generator connecting to the distribution network, in order to protect against the case that the DG continues to energize the feeder when the utility has opened-creating an unintentional island. An unintentional island, although rather unlikely in real life, could be created by one of two scenarios.

1. Result of the inadvertent opening of the substation feeder breaker/recloser or one of the protection devices further down the feeder. This could be done in error or as a planned operation where the utility personnel do not realize that there is a DG present on the line. Eventually the line is re-

energized and the risk of out-of-phase reclosing exists, if the DG remains online.

2. It would be a temporary fault that leads to operation of the utility protection device but the DG's protection does not operate before the self-clearing fault extinguishes, creating the temporary island.

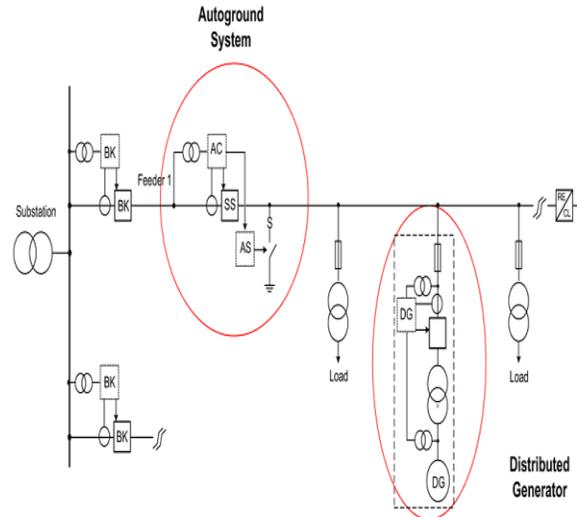


Fig. 1. Description of the autoground concept.

Fig. 1 presents the autoground concept, where the autoground system is installed just downline of the utility protection device (substation breaker or inline recloser). In this configuration, following opening of the utility breaker, the autoground opens the substation side device, denoted sectionalizing switch (SS) and closes the autogrounding switch (AS) effectively applying a three phase to ground fault.

A. Control Logic

Fig. 2 illustrates the connection of the controller to the network and the logic for opening and closing of the sectionalizing switch. It is proposed to detect the opening of the upline protection device using an undercurrent relay.

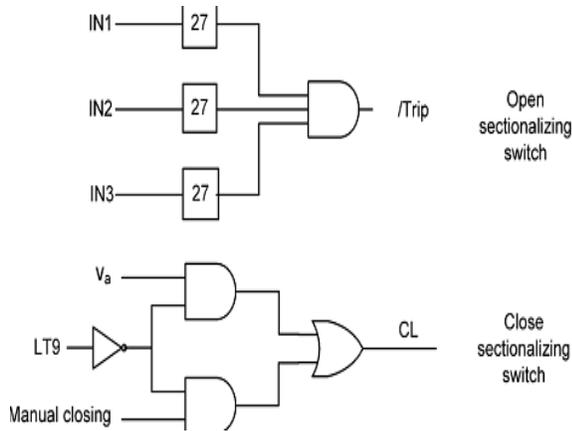


Fig. 2. Autoground sectionizing switch closing and opening logic.

III. PROPOSED SYSTEM

All DGs that have not already disconnected based on their antiislanding protection will be forced to disconnect based onlineprotection. Here it is assumed that the DG’s line protection hasbeen properly configured in order to detect all faults, as requiredby In the case of inverter based DG, over current protectionalone may not be sufficient and more advanced functions suchas over current with voltage restraint may be required.

However,the focus of the present work is on the validation of the concept.Following application of the autoground for the predefined time,it then flips states, opening AS following by closing of its SS.The utility breaker, then re-energizes the system, without a risk of out-of-phase reclosing as shown in fig.3

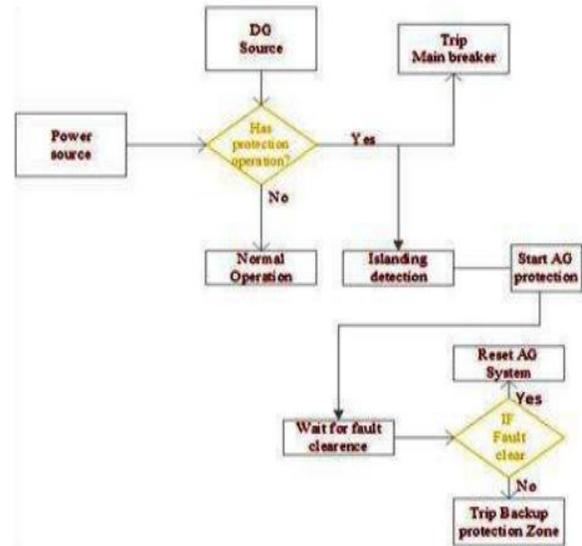


Fig.3. Flow chart of the anti-islanding protection

The autoground system consists of three main components:

- 1) Sectionalizing switch the
- 2) Autoground switch, and
- 3) Controller, which can be implemented using a variety recloser or breaker controls.

Here we describe each of these components in turn the SS is required only to mirror the state of the substation breaker. It is preferable to have the SS as a separate device for the simple reason that costs escalate when work within the substation is required. Any savings associated with the integration of the SS function into the feeder breaker would be outweighed by the cost of linking it with the AS. Illustrates the vacuum bottle based recloser used in theexperimental set-up as the SS. As the AS is connected inparallel with the distribution network only in order to applythe fault, it does not need to interrupt fault current either. As aresult, the apparatus is even simpler, and is realized by a slight modification to an automated capacitor bank assembly.Itautomatically detects the absence of a power line carrier signalwhen the distributed generator becomes electrically isolated(i.e. islanded) from the utility grid due to, for example, theopening of a breaker in the grid. With the knowledge of this situation, distributed generators are automatic disconnected fromthe grid in a timely manner for safe operation

Analysis of the corresponding equations

$$X_{fmr} FLA = (KVA * 1000) / (EL-L * 1.732) * 3-Ph I_{sc} \text{ at } X_{fmr} = (((KVA/1000) * MVA) / (1.732 * EL-L)) * 100 / Z \%$$

$$3-Ph I_{sc} \text{ at fault} = I_{sc} \text{ at } X_{fmr} *$$

Where:

EL-L = phase to phase voltage

Z = transformer nameplate impedance

IL-L-L= available 3-phase SC current

IV. SIMULATION RESULTS

The technique is conducted on proposed distribution test linemodel, configured according to the autoground system is installed at the end of the first feeder.

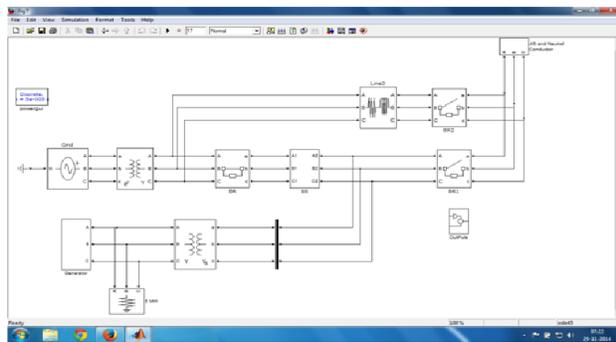


Fig.4 The Monitoring of Proposed anti islanding technique

The synchronous generator is connected to the second feeder through a 600 V/25 kV transformer, as indicated.

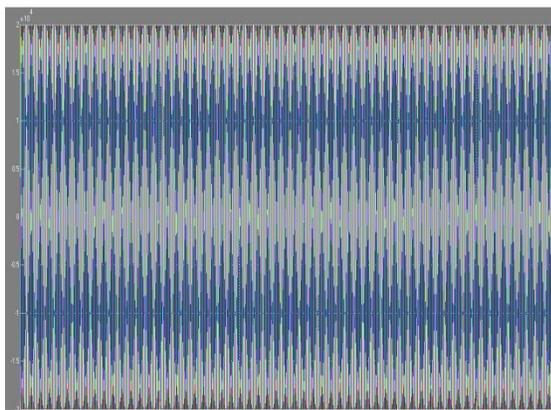


Fig.5

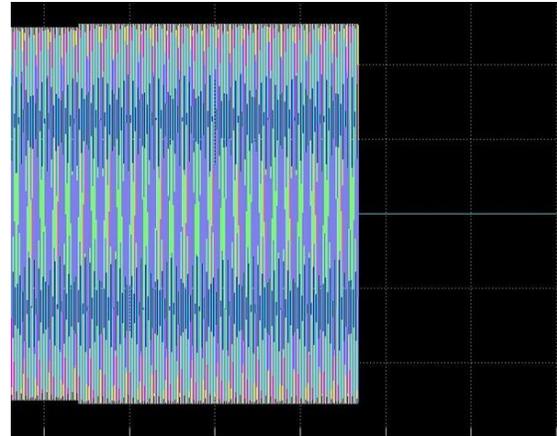


Fig.6

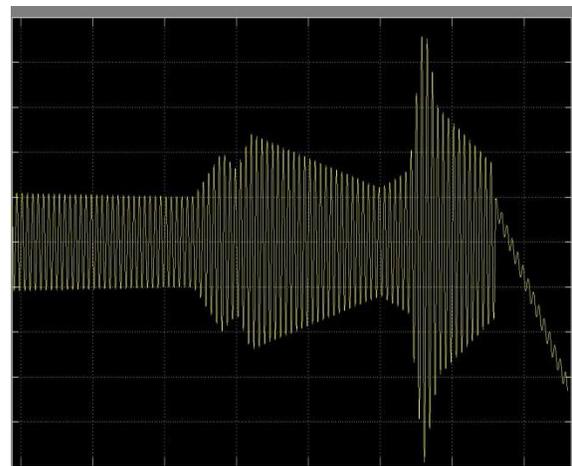


Fig.7

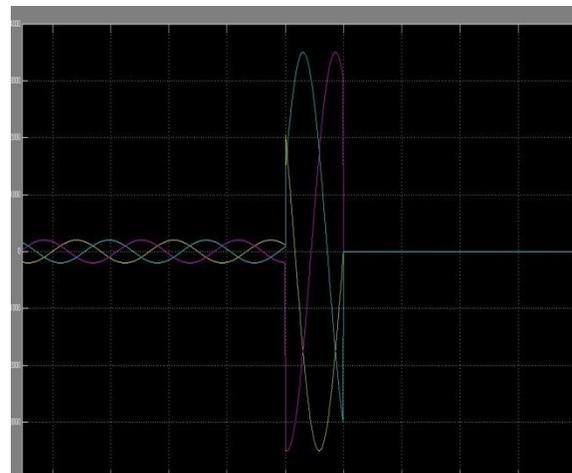


Fig.8

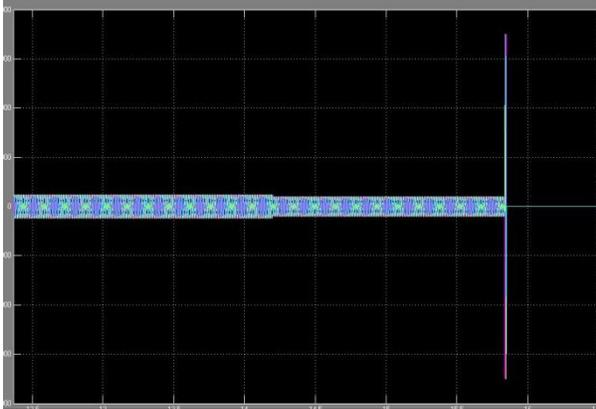


Fig.9

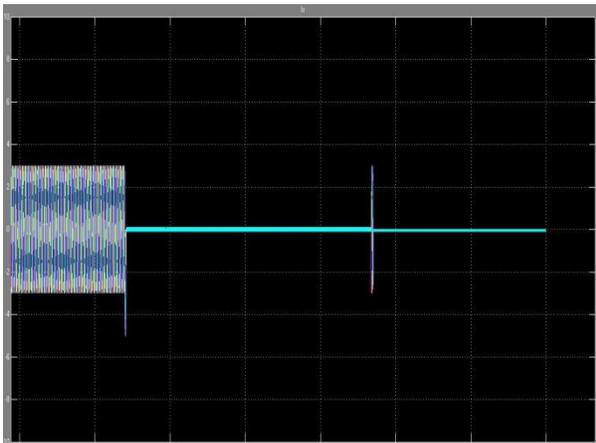


Fig.10

V. CONCLUSION

This paper is presented a new and powerful anti-islanding protection concept and associated scheme for Utility and DG applications. However, the signal is sent through power line, which makes the scheme applicable to any distribution systems regardless the availability of signal detection means. More importantly, since the signal passes through any switches, breakers and other open able components connected between the substation and DG sites; the scheme is able to detect automatically.

REFERENCES

[1] An Autoground System for Anti-Islanding Protection of DG, Chad Abbey, Member, IEEE, Yves Brissette, Senior Member, IEEE, and Philippe Venne, Member, IEEE [2] Electricity Assoc., G59/1 recommendations for the connection of embedded

generating plant to the regional electricity companies distribution systems Electricity Assoc. Std., 1991.

[3] W. Bower and M. Ropp, Evaluation of islanding detection methods for photovoltaic utility Int. Energy Agency, Rep. IEAPVPS T5-09, 2002. [Online]. Available: http://www.ojaservices.nl/iea-pvps/products/download/rep5_09.pdf.

[4] W. Xu, K. Mauch, and S. Martel, August 2004, An assessment of the islanding detection methods and distributed generation islanding issues for Canada, A report for CANMET Energy Technology Centre—Varenes, Nature Resources Canada, 65 pages. [Online]. Available:

http://www.cetcvarenes.nrcan.gc.ca/fichier.php/39002/2004-074_e.pdf.

[5] S. T. Mak, —A new method of generating TWACS type outbound signals for communication on power distribution networks, IEEE Trans. Power App. Syst., vol. PAS-103, no. 8, pp. 2134–2140, Aug. 1984.

[6] C. Abbey and P. Venne, “Field validation of a reverse reactive power relay for anti-islanding protection of a synchronous generator,” in Proc. CIGRE Canada Conf. Power Syst., Sep. 2011.

[7] Vieira, J. C. M. Vieira, W. Freitas, W. Xu, and A. Morelato, “Efficient coordination of ROCOF and frequency relays for distributed generation protection by using the application region,” IEEE Trans. Power Del., vol. 21, no. 4, pp. 1878–1884, Oct. 2006.

[8] K. El-Arroudi and G. Joos, “Data mining approach to threshold settings of islanding relays in distributed generation,” IEEE Trans. Power Syst., vol. 22, no. 3, pp. 1112–1119, Aug. 2007.

[9] S. R. Samantaray, K. El-Arroudi, G. Joos, and I. Kamwa, “A fuzzy rule-based approach for islanding detection in distributed generation,” IEEE Trans. Power Del., vol. 25, no. 3, pp. 1427–1433, Jul. 2010.

[10] W. Wang, J. Kliber, G. Zhang, W. Xu, B. Howell, and T. Palladino, “A power line signaling based scheme for anti-islanding protection of distributed generators—part II: Field test results,” IEEE Trans. Power Del., vol. 22, no. 3, pp. 1767–1772, Jul. 2007.

BIODATA

Author



R. Vinay Kumar presently pursuing his M.Tech in Electrical Power Systems from Dr.K.V.Subbareddy College of Institute &Technology, Andhra Pradesh, India.

Co-Author



D. Masthan received M.Tech. Presently working as Associate Professor in Dr.K.V.Subbareddy College of Institute &Technology, Andhra Pradesh, India.