

Removal of phosphorous from sewage treatment plant by electrocoagulation

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Abstract—Phosphorus removal from wastewater is a critical environmental concern due to its role in eutrophication. Electrocoagulation, an electrochemical water treatment method, has gained attention for its efficiency in removing phosphorus contaminants. This abstract presents an overview of the electrocoagulation process and its effectiveness in phosphorus removal. The electrocoagulation process involves the use of sacrificial electrodes to generate coagulating agents, primarily metal hydroxides, that aid in the precipitation and subsequent removal of phosphorus species. The mechanism involves destabilization of phosphorus particles through electrochemical reactions, forming flocs that are easily separated from the water. Various parameters influencing electrocoagulation's efficiency, such as pH, current density, electrode material, and electrolyte concentration, are discussed in this abstract. Optimization of these parameters is crucial for enhancing phosphorus removal efficiency while minimizing energy consumption and operational costs. Furthermore, the abstract highlights the advantages of electrocoagulation, such as its adaptability to different water qualities, relatively low sludge production, and potential for automation and integration into existing treatment processes. In conclusion, electrocoagulation exhibits significant promise as a sustainable and cost-effective method for phosphorus removal from wastewater. Continued research and technological advancements in this field hold the potential to address environmental concerns associated with phosphorus pollution effectively.

Keywords— Aluminium, Electrocoagulation, Eutrophication, Phosphate, Stainless steel

I. INTRODUCTION

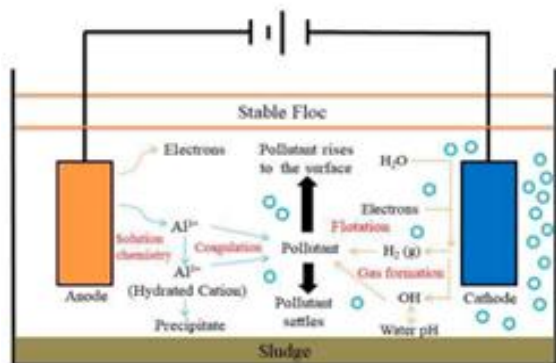
Environmental contamination caused by domestic, municipal and industrial wastewater has become a serious environmental problem which has harmful consequences on the public health. The effluent from

these industries is often responsible for severe pollution and contamination of ground water, rivers and lakes in the surrounding area (Heffron *et al.*, 2015). Phosphorus (P) is an essential element for industrial and agricultural products and found commonly in groundwater, domestic and industrial waste water (Zelmanov and Semiat., 2014). Phosphate pollution is a wide spread and challenging environmental problem because the presence of nutrients, especially nitrogen and phosphorus in wastewater effluents cause the anthropogenic phosphorus (not nitrogen) addition in milligrams per liter level to trigger algal growth. As a result, phosphorus removal to lowest level has become increasingly important. Discharge of P into the water bodies also results with the decrease of dissolved oxygen (DO), water quality deterioration, biodiversity reduction and fish death. P removal from wastewater is a complex process due to differences in its forms and in the composition of wastewater. The usual forms of P found in wastewater include orthophosphate, polyphosphate and organic phosphate. Municipal wastewater may contain 5-20 mg/L of TP. The maximum amount of P recommended for effluent discharge has been limited to 1 mg/L

II. ELECTROCOAGULATION

EC is a technology in which the coagulant is generated in situ by oxidation of a metal anode material when applying electrical current. When direct current is applied to water through a pair of electrodes, the water molecules are broken down into hydrogen and oxygen gas. The reaction is observed through the hydrogen bubbles that evolve from the cathode and oxygen bubbles that originate from the

anode. EC has occurred in three steps. In first step, coagulant has formed because of oxidation of anode. In second step, pollutants have destabilized. In last step, destabilized matters have united..



III. METHODOLOGY

The methodology for the experiment involves several steps. Initially, a sample is collected from the Karaikudi Rastha Sewage Treatment Plant, specifically from the secondary clarifier. The collected wastewater is characterized by measuring parameters such as pH, Total Dissolved Solids (TDS), Total Suspended Solids (TSS), phosphate levels, Biochemical Oxygen Demand (BOD), Chemical Oxygen Demand (COD), and electrical conductivity. A batch-scale reactor setup with a 1-liter capacity and a working volume of 750 mL is used for the experiment. The anode is made of aluminum, the cathode of stainless steel, and sodium chloride (NaCl) serves as the electrolyte. The experiment then proceeds to optimize various parameters, including current density, electrolyte concentration, and electrolysis time. Finally, the treated effluent is characterized to assess the effectiveness of the treatment process. The entire process flow is detailed in the provided flowchart, illustrating the experimental methodology.

A. Characterisation methods

The samples collected from the proposed conventional sewage treatment plant (STP) will be subjected to initial characterization for parameters which will be determined according to Standard Methods for the Examination of Water and Wastewater (APHA 2017). The parameters and standard methods used to characterize the sample are summarized in the table below.

| PARAMETERS | TEST METHODS | METHODS/ EQUIPMENTS |
|-------------------------|---------------------------------------|------------------------|
| pH | 4500-HB | pHmeter |
| Electrical conductivity | IS3025 (Part14) | Conductivitymeter |
| Chlorides | 4500-Cl-B | Argentometric method |
| Phosphate | 4500-PO ₄ ²⁻ -D | Stannouschloridemethod |
| TSS | 2520 G | Gravimetricmethod |
| TDS | 2540 C | Gravimetricmethod |

B. Discharge standards

| Sl. No | PARAMETERS | STANDARDS (except pH all values are in mg/L) | | | |
|--------|---------------------------|--|---------------|--------------------|-----------------------|
| | | Inland surface water | Public sewers | Land of irrigation | Marine/ coastal areas |
| 1. | pH | 5.5-9 | 5.5-9 | 5.5-9 | 5.5-9 |
| 2. | Suspended solids | 100 | 600 | 200 | 100 |
| 3. | BOD ₅ @ 27 ° C | 30 | 350 | 100 | 100 |
| 4. | COD | 250 | - | - | 250 |
| 5. | Dissolved phosphate as P | 5 | - | - | - |

C. Experimental Configuration

A glass beaker with a working volume of 750 ml will be used as a batch scale reactor. The aluminum electrode and stainless steel of size 50 mm × 100 mm each were used for the anode and cathode respectively. The electrodes were held 2.5 cm apart with an electrode effective area, 30 cm², submerged in the solution held in 1 L container. The schematic diagram of EC unit is shown in the fig.1



Fig 1 – Electrocoagulation reactor setup

D. Operational Parameters

- 1)Effect of supporting electrolyte
- 2)Effect on current density
- 3)Effect on reaction time

IV. RESULTS AND DISCUSSIONS

A. CHARACTERISTICS OF WASTEWATER

The secondary treated wastewater collected from the Karaikudi Rastha sewage treatment plant for which the initial characteristics are carried out and their corresponding values are tabulated in the Table 3 below

Table 3 – Influent characteristics after secondary clarifier

| Sl.No | Parameters | Values |
|-------|---------------------------------|--------|
| 1. | pH | 7.31 |
| 2. | Electrical conductivity (mS/cm) | 4.25 |
| 3. | Chlorides | 280 |
| 4. | Phosphorus | 11.2 |
| 5. | TSS | 25 |
| 6. | TDS | 360 |
| 7. | COD | 90 |
| 8. | BOD ₅ @ 27 ° C | 21 |

B. CHARACTERISATION OF WASTEWATER

Initial P concentration - (17 mg/L). Generally the P concentration in the sewage treatment plant varies from 5 to 20 mg/l. So the initial P concentration of the secondary treated sample collected from the STP was varied by adding potassium di-hydrogen orthophosphate to vary the initial P concentration to 17 mg/L, 11mg/L and 5mg/L to carry out the EC process and the operational parameter initially varied is the current. The current varied is from 0.25A and 0.50A with the corresponding current density of 8.33 mA/cm², 16.67 mA/cm² and 25 mA/cm² and after the reaction time the corresponding absorbance are noted and tabulated in Table 4, 5, 6 respectively.

Table 4 – Effect of current on phosphorous removal (I=0.25A). Electrolyte used – NaCl (2.5, 5, 7.5 mM) ABS – Absorbance @ 660nm

| TIME (MINUTES) | 2.5 mM | | 5 mM | | 7.5 mM | |
|----------------|--------|----|-------|----|--------|----|
| | ABS | % | ABS | % | ABS | % |
| 0 | 0.660 | 0 | 0.654 | 0 | 0.637 | 0 |
| 10 | 0.621 | 6 | 0.591 | 10 | 0.560 | 12 |
| 20 | 0.532 | 19 | 0.422 | 35 | 0.495 | 22 |
| 30 | 0.438 | 34 | 0.240 | 63 | 0.235 | 63 |
| 40 | 0.279 | 58 | 0.139 | 79 | 0.107 | 83 |
| 50 | 0.176 | 73 | 0.082 | 87 | 0.075 | 88 |
| 60 | 0.117 | 82 | 0.064 | 90 | 0.047 | 93 |
| 70 | 0.079 | 88 | 0.041 | 94 | 0.032 | 95 |

| | | | | | | |
|----|-------|----|-------|----|-------|----|
| 80 | 0.037 | 94 | 0.036 | 95 | 0.028 | 96 |
| 90 | 0.028 | 96 | 0.030 | 96 | 0.024 | 96 |

Table 5– Effect of current on phosphorous removal (I=0. 5A)

Electrolyte used – NaCl (2.5, 5, 7.5 mM)
ABS – Absorbance @ 660nm

| TIME (MINUTES) | 2.5 mM | | 5 mM | | 7.5 mM | |
|----------------|--------|----|-------|----|--------|----|
| | ABS | % | ABS | % | ABS | % |
| 0 | 0.634 | 0 | 0.627 | 0 | 0.634 | 0 |
| 10 | 0.451 | 29 | 0.429 | 32 | 0.307 | 52 |
| 20 | 0.391 | 38 | 0.283 | 55 | 0.168 | 74 |
| 30 | 0.304 | 52 | 0.116 | 81 | 0.067 | 88 |
| 40 | 0.174 | 73 | 0.040 | 94 | 0.035 | 94 |
| 50 | 0.078 | 88 | 0.031 | 95 | 0.029 | 95 |
| 60 | 0.059 | 91 | 0.027 | 96 | 0.027 | 96 |
| 70 | 0.029 | 95 | 0.025 | 96 | 0.023 | 96 |
| 80 | 0.021 | 97 | 0.022 | 97 | 0.019 | 97 |
| 90 | 0.018 | 97 | 0.019 | 97 | 0.016 | 98 |

The absorbance values for different initial P concentration are tabulated and their corresponding graphs are plotted as shown in the Fig 2, and 3.

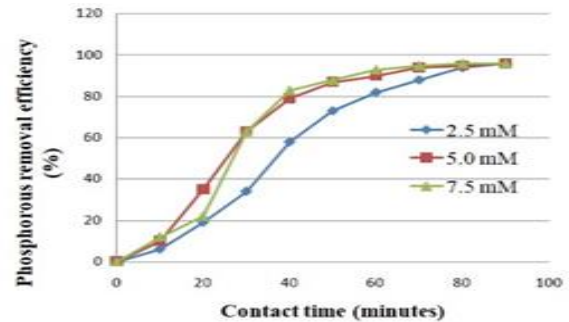


Fig 2 – Effect of 0.25A current on 17 mg/L of initial P concentration

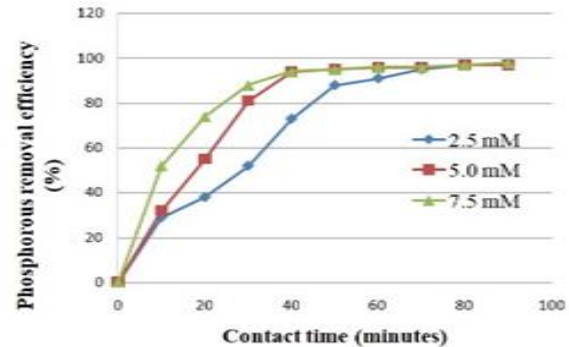


Fig 3 – Effect of 0.5A current on 17 mg/L of initial P concentration

From the above graphs it is observed that the behaviour of a phosphorus removal during the initial stages follow a linear increase this occurs when the treatment conditions are favourable and the reactions between the treatment agents i.e., the electrode-generated species in EC process and phosphorus compounds are efficient and well controlled. As the treatment progresses, several factors like competing reactions, particle agglomeration, reactor conditions can lead to fluctuating trend in P removal. Understanding these factors is important for optimizing treatment design and operational strategies. It is observed from the graph that >90% removal efficiency was achieved at 40 min in 0.5A while reducing the current to 0.25A, >90% removal was achieved in 60 min. As the current increases the removal efficiency increases with decrease in time.

Initial P concentration - (11 mg/L)

The initial P concentration for the secondary treated wastewater was varied to 11mg/L by adding potassium di-hydrogen orthophosphate and the operational parameter varied is the current from 0.25A .and.0.5A and the corresponding phosphorous absorbance at different time intervals are given in Table 6, 7respectively.

Table 6– Effect of current on phosphorous removal (I=0.25A)

Electrolyte used – NaCl (2.5, 5, 7.5 mM) ABS
– Absorbance @ 660nm

| TIME (MINUTES) | 2.5 mM | | 5 mM | | 7.5 mM | |
|----------------|--------|----|-------|----|--------|----|
| | ABS | % | ABS | % | ABS | % |
| 0 | 0.415 | 0 | 0.417 | 0 | 0.409 | 0 |
| 10 | 0.395 | 5 | 0.350 | 16 | 0.310 | 24 |
| 20 | 0.283 | 32 | 0.276 | 34 | 0.230 | 44 |
| 30 | 0.179 | 57 | 0.162 | 61 | 0.155 | 62 |
| 40 | 0.115 | 73 | 0.111 | 74 | 0.106 | 74 |
| 50 | 0.090 | 78 | 0.086 | 80 | 0.079 | 81 |
| 60 | 0.075 | 82 | 0.073 | 82 | 0.065 | 84 |
| 70 | 0.066 | 85 | 0.061 | 85 | 0.055 | 87 |
| 80 | 0.045 | 90 | 0.040 | 90 | 0.035 | 92 |
| 90 | 0.036 | 91 | 0.029 | 93 | 0.020 | 95 |

Table 7 – Effect of current on phosphorous removal (I=0.5A)

Electrolyte used – NaCl (2.5, 5, 7.5 mM)
ABS – Absorbance @ 660nm

| TIME (MINUTES) | 2.5 mM | | 5 mM | | 7.5 mM | |
|----------------|--------|----|-------|----|--------|----|
| | ABS | % | ABS | % | ABS | % |
| 0 | 0.432 | 0 | 0.415 | 0 | 0.422 | 0 |
| 10 | 0.361 | 16 | 0.342 | 18 | 0.301 | 29 |
| 20 | 0.279 | 35 | 0.265 | 36 | 0.228 | 46 |
| 30 | 0.154 | 64 | 0.138 | 67 | 0.113 | 73 |
| 40 | 0.085 | 80 | 0.062 | 85 | 0.056 | 87 |
| 50 | 0.036 | 92 | 0.034 | 92 | 0.032 | 92 |
| 60 | 0.033 | 92 | 0.030 | 93 | 0.028 | 93 |
| 70 | 0.031 | 93 | 0.026 | 94 | 0.021 | 95 |
| 80 | 0.026 | 94 | 0.025 | 94 | 0.015 | 96 |
| 90 | 0.024 | 94 | 0.023 | 95 | 0.014 | 97 |

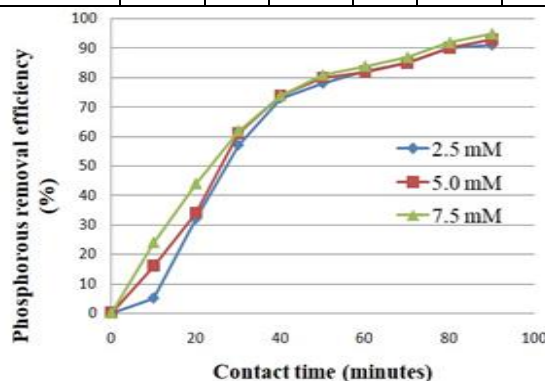


Fig 4– Effect of 0.25A current on 11 mg/L of initial P concentration

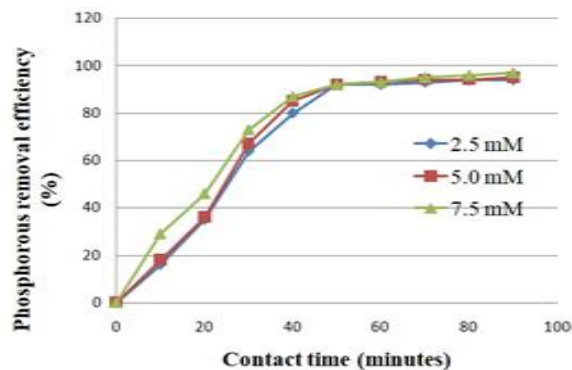


Fig 5 – Effect of 0.5A current on 11 mg/L of initial P concentration

Initial P concentration - (5 mg/L)

The initial P concentration for the secondary clarified water was varied to 5mg/L by adding potassium di-hydrogen orthophosphate and varying the current from 0.25A and 0.50A and the corresponding phosphorous absorbance at different time intervals are given in Table 8 and 9.

Table 8 – Effect of current on phosphorous removal (I=0.25A)

Electrolyte used – NaCl (2.5, 5, 7.5 mM) ABS
 – Absorbance @ 660nm

| TIME(MINUTE S) | 2.5 mM | | 5 mM | | 7.5 mM | |
|----------------|--------|----|-------|----|--------|----|
| | ABS | % | ABS | % | ABS | % |
| 0 | 0.182 | 0 | 0.185 | 0 | 0.191 | 0 |
| 10 | 0.156 | 14 | 0.150 | 19 | 0.099 | 48 |
| 20 | 0.091 | 50 | 0.084 | 55 | 0.051 | 73 |
| 30 | 0.072 | 60 | 0.066 | 64 | 0.038 | 80 |
| 40 | 0.053 | 71 | 0.045 | 76 | 0.036 | 81 |
| 50 | 0.041 | 77 | 0.039 | 79 | 0.030 | 85 |
| 60 | 0.034 | 81 | 0.031 | 84 | 0.025 | 87 |
| 70 | 0.029 | 84 | 0.028 | 85 | 0.020 | 89 |
| 80 | 0.024 | 87 | 0.025 | 87 | 0.019 | 91 |
| 90 | 0.021 | 89 | 0.022 | 91 | 0.019 | 91 |

Table 9 – Effect of current on phosphorous removal (I=0.5A)

Electrolyte used – NaCl (2.5,5,7.5 mM) ABS
 – Absorbance @ 660nm

| TIME (MINUTES) | 2.5 mM | | 5 mM | | 7.5 mM | |
|----------------|--------|----|-------|----|--------|----|
| | ABS | % | ABS | % | ABS | % |
| 0 | 0.187 | 0 | 0.191 | 0 | 0.182 | 0 |
| 10 | 0.113 | 40 | 0.128 | 33 | 0.081 | 55 |
| 20 | 0.080 | 57 | 0.077 | 60 | 0.049 | 73 |
| 30 | 0.056 | 70 | 0.033 | 83 | 0.028 | 85 |
| 40 | 0.043 | 77 | 0.031 | 84 | 0.026 | 86 |
| 50 | 0.036 | 81 | 0.029 | 85 | 0.024 | 87 |
| 60 | 0.033 | 82 | 0.024 | 87 | 0.022 | 88 |
| 70 | 0.029 | 85 | 0.020 | 90 | 0.022 | 88 |
| 80 | 0.026 | 86 | 0.019 | 90 | 0.018 | 91 |
| 90 | 0.022 | 88 | 0.017 | 91 | 0.018 | 91 |

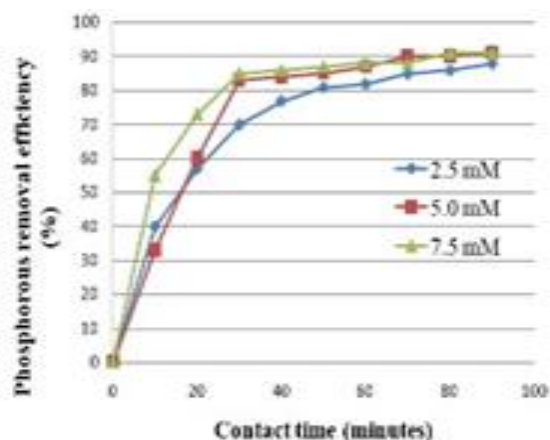


Fig 6 – Effect of 0.25A current on 5 mg/L of initial P concentration

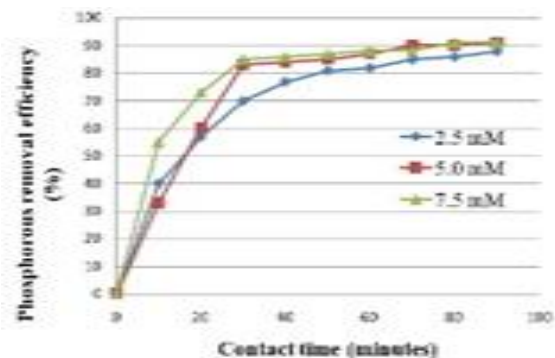


Fig 7 – Effect of 0.5A current on 5 mg/L of initial P concentration

The optimized conditions for all the 3 different initial P concentrations are to be found out by considering the P removal efficiency, electrolyte dosage, current density, reaction time, energy consumption, amount of P adsorbed and sludge quantity. Table 10 shown below gives the optimized condition values.

Table 10 – To determine the optimized condition

| Initial PP concentration (mg/L) | Current density (mA/cm ²) | Electrolyte dosage (mM) | Time (min) | Cen(k Wh/m ³) | Cp(m g P/g Al) | Sludge quantity (g/m ³) |
|---------------------------------|---------------------------------------|-------------------------|------------|---------------------------|----------------|-------------------------------------|
| 17 | 16.67 | 5 | 40 | 5.55 | 52.07 | 978.67 |
| 11 | 16.67 | 2.5 | 50 | 9.45 | 43.91 | 824 |
| 5 | 16.67 | 5 | 30 | 4.66 | 40.87 | 900 |

A. EFFLUENT CHARACTERISATION

In order to check the EC treated effluent the final characteristics of the effluent are done and given in Table 11.

Table 11 – Effluent characteristics after treatment(All the values mentioned below are in mg/L except pH)

| Sl. No. | Parameters | Initial phosphorus concentration (mg/L) | | |
|---------|---------------------------------|---|-------|-------|
| | | 17 | 11 | 5 |
| 1. | pH | 7.3 | 7.1 | 7.3 |
| 2. | Electrical conductivity (mS/cm) | 1.420 | 1.195 | 0.882 |
| 3. | TDS | 350 | 330 | 325 |
| 4. | Chloride | 245 | 240 | 238 |
| 5. | Phosphorus | 0.96 | 0.94 | 0.87 |
| 6. | COD | 15 | 12 | 18 |
| 7. | BOD5 @ 27 °C | 9 | 9 | 12 |

V.CONCLUSION

Phosphorus is usually the main limiting nutrient for eutrophication in inland receiving water bodies; therefore, P concentration must be controlled. The purpose of this study was to investigate the effectiveness of EC process using aluminum and stainless steel electrodes for the phosphorus removal of the secondary treated wastewater. 94% P removal efficiency was achieved for 17mg/L of initial P concentration similarly 92 % for 11mg/L and 85% for 5 mg/L.

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